

Whole-Body Control for Robots in the Real World

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# Inverse Kinematics: New Method for Minimum Jerk Trajectory Generation

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# Inverse Kinematics Problem

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- Formulation and classical resolution

- Original optimization problem :  $\min_{\dot{q}} \dot{q}_t^T Q \dot{q}_t$  subject to  $J \dot{q}_t = \dot{r}_t$

➔ Minimize joints velocity.

- Pseudo-inverse technique :  $\dot{q}_t = J^+ \dot{r}_t$  with  $J^+ = J^T (J J^T)^{-1}$

➔ **Joints velocity** as the control parameter.

- Additional constraints

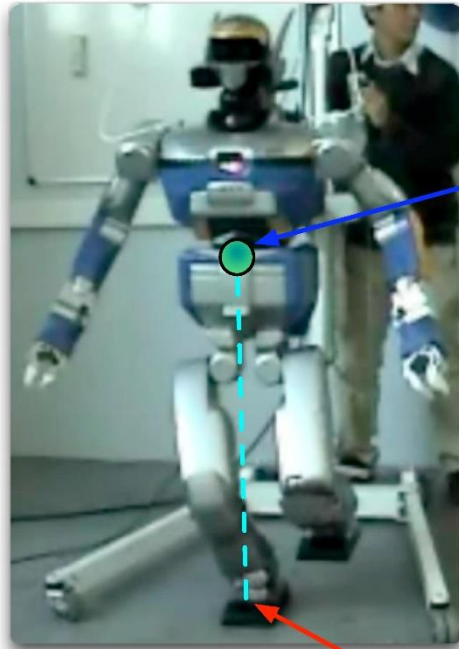
- Velocity/joints limits and obstacles inequality :  $A \dot{q}_t \leq b$
- Quadratic Programming (QP) solver.

- **No constraints** on the **acceleration** or the **jerk**

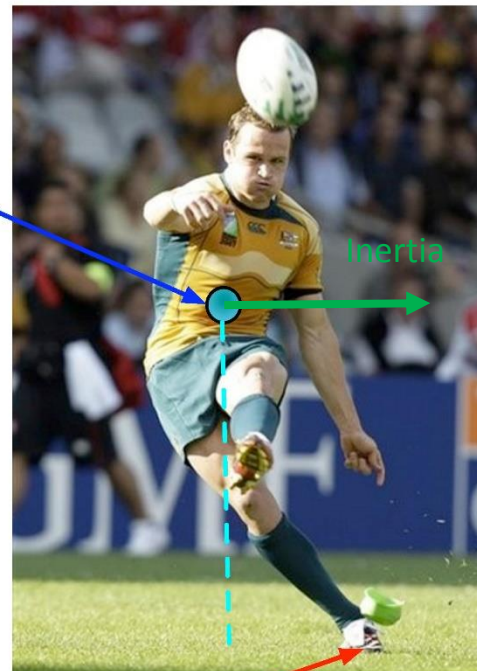
# Zero Moment Point (ZMP)

- Humanoid robots dynamic stability control.

Statically stable



Dynamically stable



Center of Mass (CoM)

Inertia

ZMP

- Stability  $\leftrightarrow$  ZMP inside the polygon of support.
- ZMP depends on joint accelerations.

Discontinuous accelerations



Discontinuous ZMP trajectory



Imbalance

# Joints jerk control

- Objective : To keep joints jerk within bounds for continuous acceleration.
- Relation between position, velocity, acceleration and jerk :

$$\begin{bmatrix} q_t \\ \dot{q}_t \\ \ddot{q}_t \end{bmatrix} = \begin{bmatrix} I_n & T I_n & \frac{T^2}{2} I_n \\ 0 & I_n & T I_n \\ 0 & 0 & I_n \end{bmatrix} \begin{bmatrix} q_{t-1} \\ \dot{q}_{t-1} \\ \ddot{q}_{t-1} \end{bmatrix} + \begin{bmatrix} \frac{T^3}{6} I_n \\ \frac{T^2}{2} I_n \\ T I_n \end{bmatrix} \ddot{q}_t = u_t \text{ (control)}$$

$= X_t$  (Vector to be computed)  $= X_{t-1}$  (Current configuration)

→  $\dot{q}_t = \dot{q}_{t-1} + T \ddot{q}_{t-1} + \frac{T^2}{2} u_t$  Relationship between **velocity** and **jerk**

# Problem reformulation

$$\begin{aligned} \min_{\dot{q}} \quad & \dot{q}_t^T Q \dot{q}_t \\ \text{subject to} \quad & \\ & J \dot{q}_t = \dot{r}_t \\ & A \dot{q}_t \leq b \end{aligned}$$

$$\dot{q}_t = \dot{q}_{t-1} + T \ddot{q}_{t-1} + \frac{T^2}{2} u_t$$



$$\min_{u_t} u_t^T Q u_t$$

subject to

$$J u_t = \tilde{r}_t$$

$$A u_t \leq \tilde{b}$$

$$u^- \leq u_t \leq u^+$$

Limits of the  
jerk vector

Where :


$$\tilde{r}_t = \frac{2}{T^2} (\dot{r}_t - J \dot{q}_{t-1} - J T \ddot{q}_{t-1})$$

$$\tilde{b} = \frac{2}{T^2} (b - A \dot{q}_{t-1} - A T \ddot{q}_{t-1})$$

# Implementation

## Control algorithm


$r_{t-T}, X_{t-T}$



$X_0 = \begin{bmatrix} q_0 \\ 0 \\ 0 \end{bmatrix}$   
 $t = T$


$$J = f(r_{t-T}, q_{t-T})$$

$J, X_{t-T}$



$$\begin{aligned} & \min_{u_t} u_t^T Q u_t \\ & \text{subject to} \\ & J u_t = \tilde{r}_t \\ & A u_t \leq \tilde{b} \\ & u^- \leq u_t \leq u^+ \end{aligned}$$

$\ddot{q}, X_{t-T}$



$$\begin{bmatrix} q_t \\ \dot{q}_t \\ \ddot{q}_t \end{bmatrix} = \begin{bmatrix} I_n & T I_n & \frac{T^2}{2} I_n \\ 0 & I_n & T I_n \\ 0 & 0 & I_n \end{bmatrix} \begin{bmatrix} q_{t-1} \\ \dot{q}_{t-1} \\ \ddot{q}_{t-1} \end{bmatrix} + \begin{bmatrix} \frac{T^3}{6} I_n \\ \frac{T^2}{2} I_n \\ T I_n \end{bmatrix} \ddot{q}_t$$

$X_t$



# Experimental results

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- Objectives:

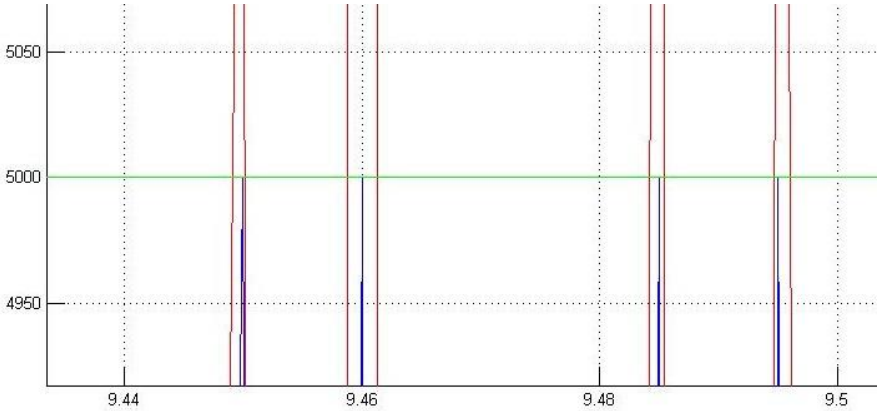
- Execute a boxing motion.
- Follow end-effector Cartesian trajectory.
- Respect limits on jerk ( $5000 \text{ rad s}^{-3}$ ).

- Tools:

- Virtual robot HRP-2 using OpenHRP platform.
- Data treatment on Matlab.

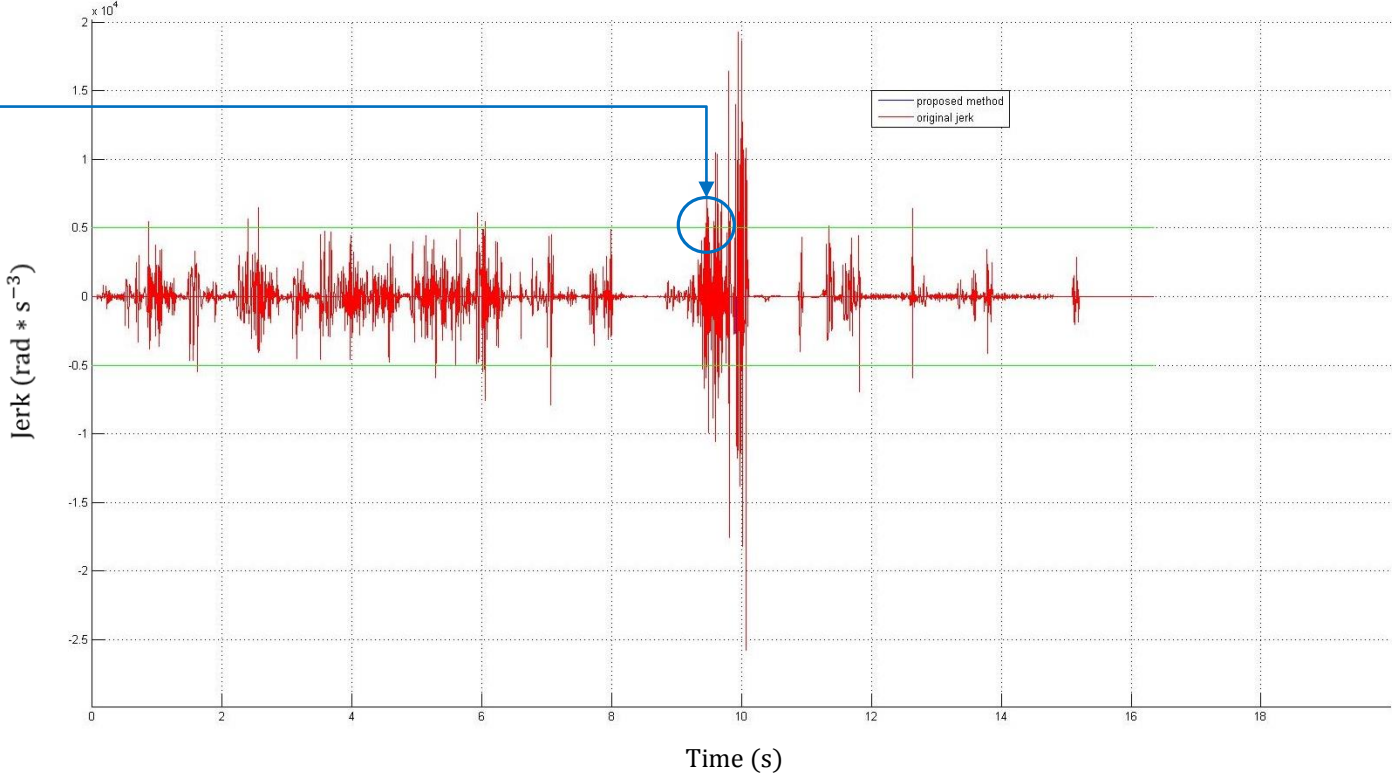


# Experimental results



Zoom on jerk limitation effects

Jerk comparison



# Conclusion

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- Advantage of the method: smooth acceleration trajectories
  - Stability of humanoid robots.
  - Less stress on the joints motors.
- Future work
  - Real-time implementation of the algorithm.
  - Validation on walking patterns while avoiding self-collision.
  - Validation on the real humanoid robot HRP-2